

LOWERING OF THE BREAKDOWN POTENTIAL  
OF A GAS UNDER STEADY IONIZING RADIATION

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The problem of the lowering of the electric strength of a gas under steady external ionizing radiation is solved numerically. The right-hand branches of the Paschen curve for helium, argon, and xenon are calculated by the so-called ranging method using the standard Runge-Kutta program.

The development of various automatic control systems for nuclear power plants requires an estimate of the working lifetime of gas-discharge devices exposed to dose rates  $P_\gamma \sim 10^2 - 10^5$  P/sec in the gamma radiation field of a reactor. Under these conditions one of the critical parameters is the electric strength.

The book [1] lists a long bibliography of papers devoted to the theoretical and experimental studies of the effect of radiation on the change in the breakdown potential of a gap. Calculations by Rogowski and his coworkers show that the relative lowering of the breakdown potential  $\eta = (U_0 - U_*)/U_0$ , where  $U_0$  is the static breakdown potential neglecting space charge and  $U_*$  is the breakdown potential in the presence of a photoelectric cathode emission current  $I_0$ , is proportional to  $\sqrt{I_0}$ . This result is derived by applying perturbation theory and expanding the system of equations in series in terms of the small parameter  $\Delta E = E(x) - E_0$ , where  $E_0$  is the initial homogeneous field for plane geometry of the electrodes and  $E(x)$  is the field deformed by the space charge when the current is  $I_0$ . Therefore the range of applicability of the relation  $\eta \sim \sqrt{I_0}$  is limited by the condition  $\Delta E \ll E_0$ , and  $\eta \ll 1$ .

In the case under consideration ionizing radiation leads to a severe deformation of the field and perturbation theory is not applicable. Since there is no exact analytical solution for the motion of particles in a self-consistent inhomogeneous field taking account of impact ionization, we calculate the dependence of the breakdown potential of a gap on the dose rate  $P_\gamma$  numerically by computer.

In plane geometry the system of equations describing the drift of particles in an inhomogeneous field taking account of impact ionization and the creation of particles by a uniform external source has the form

$$\frac{dj_e}{dx} = -\alpha(E)j_e + Q; \quad \frac{dE}{dx} = \frac{4\pi}{v_+(E)} \left( j - j_e \left( 1 + \frac{v_+(E)}{v_e(E)} \right) \right), \quad (1)$$

where  $j$  is the total current density,  $j_e$  is the electron current density,  $E$  is the electric field,  $v_+$  and  $v_e$  are the drift velocities of positive ions and electrons,  $\alpha(E)$  is the coefficient of impact ionization, and  $Q$  is the charge created by the external source per unit volume of gas per unit time; the origin of coordinates is at the anode. The parameters of the problem are  $j$  and  $Q$ .

For inert gases and an uncontaminated cathode secondary avalanches are produced mainly by ions [2], and therefore the boundary condition has the form

$$j_e(d) = \frac{\gamma_+ j}{1 + \gamma_+}, \quad j_e(0) = j, \quad (2)$$

where  $\gamma_+$  is the coefficient of secondary ionization by ions. In order to solve system (1) it is necessary to specify explicitly the form of the functions  $\alpha(E)$  and  $v_{+e}(E)$ . By interpolation of experimental data for the drift velocity of ions in inert gases Kagan and Perel' [3] obtained empirical expressions of the form

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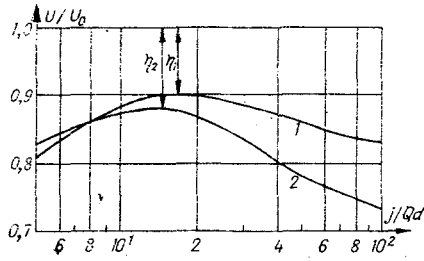


Fig. 1

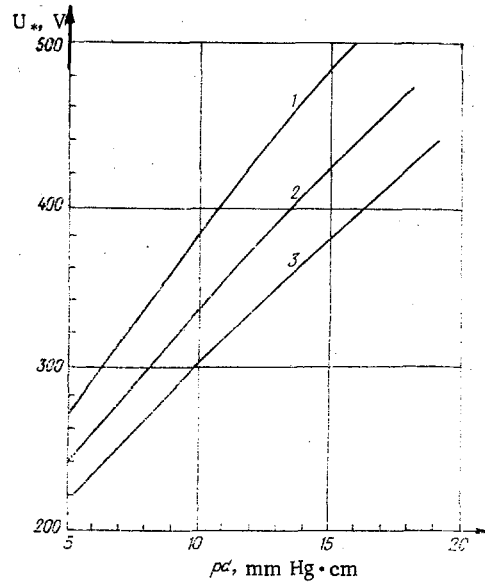


Fig. 2

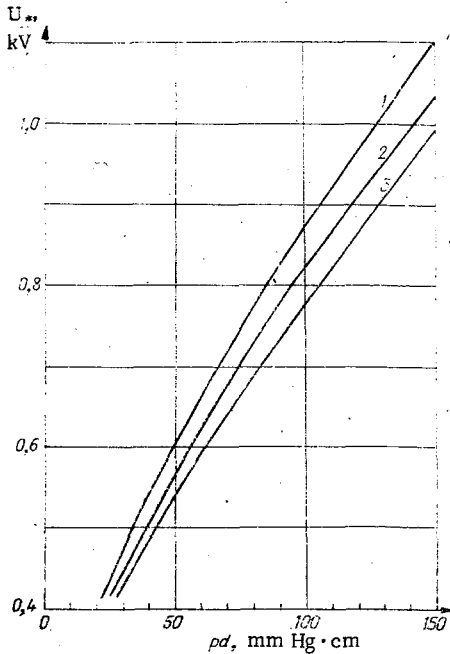


Fig. 3

$$v_+(E) = K_+ \frac{E}{p} \left(1 - C \frac{E}{p}\right), \quad \frac{E}{p} < D; \quad (3)$$

$$v_+(E) = K'_+ \left(\frac{E}{p}\right)^{1/2} \left(1 - C' \left(\frac{p}{E}\right)^{3/2}\right), \quad \frac{E}{p} > D,$$

where  $p$  is the pressure and  $K_+$ ,  $K'_+$ ,  $C$ ,  $C'$ , and  $D$  are constants for a given gas. The mobility of positive ions in inert gases has been found analytically also [4]. We used Eqs. (3) in our numerical solutions since they are in satisfactory agreement with the experimental data. In contrast with  $v_+$  we can limit ourselves to the linear approximation  $v_e = K_e (E/p)$  for the drift velocity of electrons since  $v_e$  enters system (1) as a small correction of the order  $v_+(E)/v_e$ . Ward [3] showed that the expression

$$\alpha\left(\frac{E}{p}\right) = Ap \exp\left\{-B\sqrt{\frac{p}{E}}\right\}, \quad \frac{E}{p} < W \quad (4)$$

for the coefficient  $\alpha(E)$  is valid over a wide range of values of  $E/p$  for inert gases. The numerical values of the constants in Eqs. (3) and (4) are given by Ward [3]. Thus system (1), (2) together with Eqs. (3) and (4) completely determines the problem.

The determination of the breakdown potential  $U_*$  reduces to the calculation of the volt-ampere characteristic  $U = U(j)$  for a given  $Q$ , where  $U_*$  is found from the condition  $dU/dj = 0$  [5].

System (1) together with boundary condition (2) is a two-point boundary-value problem for a system of ordinary differential equations (of the two variables  $E$  and  $j_e$  only the boundary values for  $j_e$  are given at two points). One method for solving system (1), (2) numerically is to specify another variable  $E(x = 0)$  at  $x = 0$  in a relatively arbitrary way. Since now two functions are specified at  $x = 0$  the solution can be obtained by using any standard program. We used the Runge-Kutta program. The choice of the function  $E(x = 0)$  is continued until the solution obtained for  $j_e(x = d)$  agrees with the boundary value  $\gamma_+ j / (1 + \gamma_+)$  to an a priori specified accuracy. By integrating the distribution of the field over the interval  $(0, d)$  the value of the potential corresponding to the given  $j$  and  $Q$  can be obtained. By specifying other values of  $j$  and  $Q$  and repeating the calculation ab initio the volt-ampere characteristic  $U = U(j)$  can be computed for various values of  $Q$ . This calculational procedure as applied to gas-discharge problems was first used by

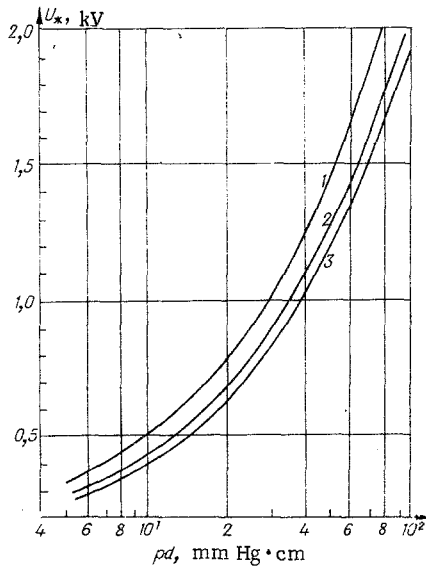


Fig. 4

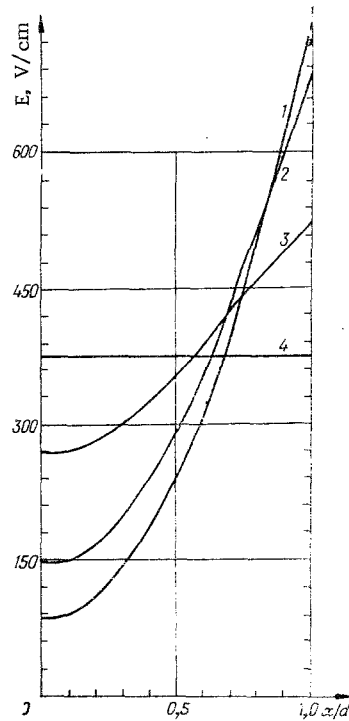


Fig. 5

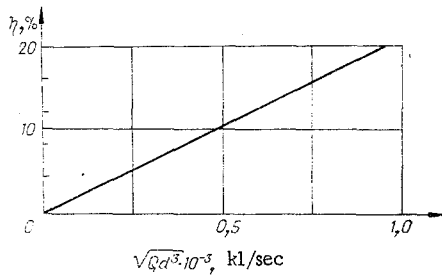


Fig. 6

Ward [6] to estimate the cathode fall in a glow discharge. Figure 1 shows the calculated volt-ampere characteristics for argon with  $Q = (1/3) \cdot 10^{-6}$ ,  $d = 1$ , and  $p = 5$  (curve 1), and for  $p = 10$  (curve 2) (in the text and on the figures the units are: V, cm, mm of Hg, Kl, sec). The ordinate is the potential relative to the static breakdown potential  $U$  determined from the condition  $\mu = \gamma_+ (\exp(\alpha_0 d) - 1) = 1$ , where  $\alpha_0$  is the coefficient of impact ionization in the field  $E_0$ . Taking account of (4) the condition  $\mu = 1$  has the form

$$U_0 = pdB^2 \left[ \ln(pdA) - \ln \ln \left( 1 + \frac{1}{\gamma_+} \right) \right]^{-2} \quad (5)$$

In all the calculations the coefficient of secondary ionization  $\gamma_+$  was taken as 0.02. The relative lowering of the breakdown potential  $\eta$  is determined from Fig. 1 as the difference  $1 - (U/U_0)_{\max}$ . If the system (1), (2) is reduced to dimensionless form, dimensional arguments show that the breakdown potential  $U_*$  depends on the parameter  $d^3 Q$  as well as on the dimensional combination  $pd$ ; i.e.,  $U_* = U_*(pd, d^3 Q)$ . By determining the maximum of the volt-ampere characteristic for various choices of the parameters  $pd$  and  $d^3 Q$  the dependence of  $U_*$  on  $pd$  can be constructed for various  $d^3 Q$ . Figure 2 shows the right-hand branch of the Paschen curve for argon [curve 1 neglects space charge, Eq. (5), curve 2 corresponds to  $d^3 Q = (1/3) \cdot 10^{-6}$ ; for curve 3  $d^3 Q = 10^{-6}$ ]. Similar curves for xenon and helium are shown in Figs. 3 and 4 using the same notation as in Fig. 2. Calculations show that in the cases under consideration  $\eta$  can have values of tens of percent. The calculational method described permits the determination of  $\eta$  as a function of  $Q$ . If we neglect the contribution to  $Q$  from secondary processes in the sheath separating the gas gap from the surrounding space the relation between  $P_\gamma$  and  $Q$  has the form [7]

$$P_\gamma = aQ[a = 5.5 \cdot 10^{26}(\lambda_1 \omega / \lambda_1)],$$

where  $\lambda_1$  and  $\lambda_2$  are the average linear energy-transfer coefficients for air at standard pressure and the filling gas at the pressure  $P$ , which is of interest to us, in cm,  $\omega$  is the energy of ion formation in the filling gas, J/ion, and  $Q$  is in  $\text{kl/cm}^3 \cdot \text{sec}$ . For example, for  $E_\gamma \sim 1$  MeV we find for argon  $a = 1.2 \cdot 10^{12}/p$  so that curves 1 and 2 in Fig. 1 correspond to  $P_\gamma = 8 \cdot 10^4$  R/sec and  $P_\gamma = 4 \cdot 10^4$  R/sec.

The mechanism for lowering the breakdown potential is explained by the increase in the multiplication factor from the deformation of the field by the space charge. Figure 5 shows the field distribution for

ignition currents  $j_*$  corresponding to various values of  $Q$  [argon  $d = 1$ ,  $p = 10$ ; curve 4 gives the initial homogeneous field; curve 3 corresponds to  $d^3 Q = (1/3) \cdot 10^{-7}$ , curve 2, to  $d^3 Q = (1/3) \cdot 10^{-6}$ , and curve 1, to  $d^3 Q = 10^{-6}$ ]. For such an inhomogeneity of the field a relation of the form  $\eta \sim \sqrt{Q}$ , which can be derived within the framework of perturbation theory when  $E(x) - E_0 \ll E_0$  and  $\eta \ll 1$ , is not applicable. However, from Fig. 6 which shows  $\eta$  as a function of  $\sqrt{d^3 Q}$  (argon  $pd = 10$ ) it is clear that the dependence is linear in the region of the values of  $Q$  which are of interest to us up to  $\eta \approx 22\%$ . The generalization of the calculation to the case  $\gamma_+ = \gamma_+(E)$  is not difficult in principle and can be done as in [8].

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